

· 基础研究 ·

上中胸椎经椎弓根 - 肋骨单元途径置钉的安全性及稳定性研究

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摘要 目的:探讨上中胸椎经椎弓根 - 肋骨单元(pedicle rib unit, PRU)途径置钉的安全性及稳定性。**方法:**对 10 名无脊柱病变的志愿者进行脊柱 T₁ ~ T₈ 节段 CT 扫描,在获得的 CT 图像上测定各节段的 PRU 途径置钉安全角度范围、椎弓根横径、PRU 横径、椎弓根纵径、PRU 纵径及 PRU 重叠纵径。取 4 具尸体脊柱标本(T₁ ~ T₈ 节段),对应肋骨保留 10 cm 左右。随机于每个脊柱标本的两侧分别经经典椎弓根途径和 PRU 途径置入椎弓根螺钉,两侧螺钉的直径及长度分别为对应的椎弓根横径的 70% 和各自钉道最长值的 70%。应用 Instron 5569 电子万能试验机测定螺钉的抗拔出力。**结果:**10 名志愿者 T₁ ~ T₈ 经 PRU 途径置钉的安全角度范围分别为 19.71° ± 1.64°、19.42° ± 1.88°、17.17° ± 0.67°、17.22° ± 1.17°、19.36° ± 1.31°、18.67° ± 1.58°、18.82° ± 2.60°、18.72° ± 1.58°。10 名志愿者 T₁ ~ T₈ 椎弓根横径均小于同节段的 PRU 横径[(8.78 ± 0.05) mm, (18.23 ± 2.46) mm, t = 18.192, P = 0.013; (7.59 ± 0.08) mm, (16.80 ± 1.31) mm, t = 20.175, P = 0.002; (6.29 ± 0.07) mm, (15.12 ± 1.22) mm, t = 20.271, P = 0.004; (5.50 ± 0.05) mm, (14.43 ± 1.00) mm, t = 27.403, P = 0.004; (5.52 ± 0.06) mm, (14.02 ± 0.85) mm, t = 20.312, P = 0.001; (5.90 ± 0.06) mm, (14.19 ± 1.12) mm, t = 16.772, P = 0.047; (6.31 ± 0.07) mm, (14.77 ± 1.31) mm, t = 14.229, P = 0.017; (6.64 ± 0.03) mm, (15.53 ± 1.90) mm, t = 13.000, P = 0.048]。10 名志愿者 T₁ ~ T₈ 椎弓根纵径、PRU 纵径、PRU 重叠纵径三者之间总体比较,差异均有统计学意义[(8.04 ± 1.01) mm, (11.05 ± 1.83) mm, (6.37 ± 0.68) mm, F = 236.422, P = 0.000; (10.72 ± 0.99) mm, (13.09 ± 1.30) mm, (7.46 ± 1.12) mm, F = 60.570, P = 0.000; (11.34 ± 0.99) mm, (13.45 ± 0.92) mm, (8.99 ± 0.62) mm, F = 67.560, P = 0.000; (10.67 ± 0.91) mm, (12.49 ± 0.94) mm, (7.94 ± 0.84) mm, F = 64.965, P = 0.000; (10.34 ± 0.94) mm, (11.96 ± 0.95) mm, (7.96 ± 0.96) mm, F = 44.926, P = 0.000; (11.33 ± 0.96) mm, (12.36 ± 0.62) mm, (7.72 ± 0.88) mm, F = 85.197, P = 0.000; (11.30 ± 0.82) mm, (12.16 ± 0.71) mm, (8.34 ± 0.47) mm, F = 92.350, P = 0.000; (11.39 ± 0.78) mm, (13.71 ± 1.51) mm, (9.34 ± 0.93) mm, F = 37.867, P = 0.000]。T₁ ~ T₈ 椎弓根纵径和 PRU 纵径均大于 PRU 重叠纵径(P = 0.004, P = 0.003, P = 0.001, P = 0.002, P = 0.013, P = 0.030, P = 0.025, P = 0.001; P = 0.000, P = 0.000)。椎弓根纵径均小于 PRU 纵径(P = 0.000, P = 0.000)。T₁ ~ T₈ 各节段经椎弓根途径置入螺钉的抗拔出力均大于经 PRU 途径[(663.60 ± 22.13) N, (470.33 ± 33.09) N, t = 27.876, P = 0.000; (702.82 ± 24.23) N, (531.76 ± 13.53) N, t = 38.402, P = 0.000; (713.58 ± 37.90) N, (544.98 ± 14.22) N, t = 37.518, P = 0.000; (700.70 ± 35.66) N, (590.80 ± 24.72) N, t = 10.512, P = 0.000; (805.28 ± 64.67) N, (591.50 ± 62.55) N, t = 19.546, P = 0.000; (808.68 ± 42.84) N, (629.08 ± 43.09) N, t = 19.436, P = 0.000; (864.62 ± 35.49) N, (591.60 ± 52.91) N, t = 24.350, P = 0.000; (909.18 ± 46.05) N, (640.70 ± 21.41) N, t = 15.162, P = 0.000]。结论:上中胸椎经 PRU 途径置入椎弓根螺钉的安全性优于经椎弓根途径,但置入螺钉的稳定性不及后者。

关键词 胸椎;椎弓根;椎弓根 - 肋骨单元;骨折固定术,内

Study on the safety and stability of upper - middle thoracic pedicle screw insertion through pedicle rib unit approach

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ABSTRACT Objective: To explore the safety and stability of upper - middle thoracic pedicle screw insertion through pedicle rib unit (PRU) approach. **Methods:** Ten volunteers with no spinal disease received CT scanning at T₁~T₈ vertebral segments, and safe angle range of pedicle screw insertion through PRU approach, transverse diameter of pedicle of vertebral arch, transverse diameter of PRU, longitudinal

基金项目:全国名老中医药专家传承工作室建设项目[国中医药人教发 2014(20)号]

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diameter of pedicle of vertebral arch, longitudinal diameter of PRU and PRU overlapped longitudinal diameter of all segments were measured on the obtained CT images. Four cadaveric T_{1~8} specimens were selected and 10 cm long ribs were reserved. The pedicle screws were randomly inserted into both sides of each spine specimen through classical pedicle of vertebral arch approach and PRU approach respectively. The diameters of the screws were 70% of transverse diameter of corresponding pedicles of vertebral arch and the lengths of the screws were 70% of the maximal values of corresponding screw path lengths. The pull-out strength of the screws were measured by using Instron 5569 electronic universal testing machine. **Results:** The safe angle ranges of pedicle screw insertion through PRU approach were 19.71 ± 1.64, 19.42 ± 1.88, 17.17 ± 0.67, 17.22 ± 1.17, 19.36 ± 1.31, 18.67 ± 1.58, 18.82 ± 2.60, 18.72 ± 1.58 degrees respectively at T_{1~8} vertebral segments of 10 volunteers. The transverse diameters of pedicle of vertebral arch were less than the transverse diameter of PRU at T_{1~8} vertebral segments of the 10 volunteers (8.78 ± 0.05 vs 18.23 ± 2.46 mm, t = 18.192, P = 0.013; 7.59 ± 0.08 vs 16.80 ± 1.31 mm, t = 20.175, P = 0.002; 6.29 ± 0.07 vs 15.12 ± 1.22 mm, t = 20.271, P = 0.004; 5.50 ± 0.05 vs 14.43 ± 1.00 mm, t = 27.403, P = 0.004; 5.52 ± 0.06 vs 14.02 ± 0.85 mm, t = 20.312, P = 0.001; 5.90 ± 0.06 vs 14.19 ± 1.12 mm, t = 16.772, P = 0.047; 6.31 ± 0.07 vs 14.77 ± 1.31 mm, t = 14.229, P = 0.017; 6.64 ± 0.03 vs 15.53 ± 1.90 mm, t = 13.000, P = 0.048). In general, there was statistical difference between longitudinal diameter of pedicle of vertebral arch, longitudinal diameter of PRU and PRU overlapped longitudinal diameter at T_{1~8} vertebral segments of the 10 volunteers (8.04 ± 1.01, 11.05 ± 1.83, 6.37 ± 0.68 mm, F = 236.422, P = 0.000; 10.72 ± 0.99, 13.09 ± 1.30, 7.46 ± 1.12 mm, F = 60.570, P = 0.000; 11.34 ± 0.99, 13.45 ± 0.92, 8.99 ± 0.62 mm, F = 67.560, P = 0.000; 10.67 ± 0.91, 12.49 ± 0.94, 7.94 ± 0.84 mm, F = 64.965, P = 0.000; 10.34 ± 0.94, 11.96 ± 0.95, 7.96 ± 0.96 mm, F = 44.926, P = 0.000; 11.33 ± 0.96, 12.36 ± 0.62, 7.72 ± 0.88 mm, F = 85.197, P = 0.000; 11.30 ± 0.82, 12.16 ± 0.71, 8.34 ± 0.47 mm, F = 92.350, P = 0.000; 11.39 ± 0.78, 13.71 ± 1.51, 9.34 ± 0.93 mm, F = 37.867, P = 0.000). The longitudinal diameter of pedicle of vertebral arch and the longitudinal diameter of PRU were larger than PRU overlapped longitudinal diameter of the 10 volunteers at T_{1~8} vertebral segments (P = 0.004, P = 0.003, P = 0.001, P = 0.002, P = 0.013, P = 0.030, P = 0.025, P = 0.001; P = 0.000, P = 0.000), and the longitudinal diameter of pedicle of vertebral arch was less than longitudinal diameter of PRU (P = 0.000, P = 0.000). The pull-out strengths of the screws inserted through the pedicle of vertebral arch approach were greater than those through PRU approach at T_{1~8} vertebral segments (663.60 ± 22.13 vs 470.33 ± 33.09 N, t = 27.876, P = 0.000; 702.82 ± 24.23 vs 531.76 ± 13.53 N, t = 38.402, P = 0.000; 713.58 ± 37.90 vs 544.98 ± 14.22 N, t = 37.518, P = 0.000; 700.70 ± 35.66 vs 590.80 ± 24.72 N, t = 10.512, P = 0.000; 805.28 ± 64.67 vs 591.50 ± 62.55 N, t = 19.546, P = 0.000; 808.68 ± 42.84 vs 629.08 ± 43.09 N, t = 19.436, P = 0.000; 864.62 ± 35.49 vs 591.60 ± 52.91 N, t = 24.350, P = 0.000; 909.18 ± 46.05 vs 640.70 ± 21.41 N, t = 15.162, P = 0.000). **Conclusion:** PRU approach surpasses pedicle of vertebral arch approach in the safety of upper-middle thoracic pedicle screw insertion, however, the latter surpasses the former in the stability of inserted screws.

Key words thoracic vertebrae; pedicle of vertebral arch; pedicle rib unit; fracture fixation, internal

椎弓根螺钉技术为下胸椎及腰椎后路内固定手术的首选^[1],上中胸椎由于椎弓根狭小,椎弓根螺钉固定的难度和风险较大^[2]。为解决这一问题,2004年Husted等^[3]提出了经椎弓根-肋骨单元(pedicle rib unit,PRU)途径置钉的理念,并已在临床应用。本研究通过影像学测量和人尸体胸椎标本模型对上中胸椎经PRU途径置钉的安全性及稳定性进行了评价,现总结报告如下。

1 材料与仪器

1.1 研究对象 10名志愿者均为在浙江省立同德医院就诊的患者。男5名,女5名;年龄30~60岁,中位数48.5岁。均无脊柱外伤史,未合并脊柱退变

性疾病、肿瘤和骨质增生及脊柱畸形。4具尸体脊柱标本(T_{1~T₈}节段),对应肋骨保留10cm左右,男性2具、女性2具。尸体标本由浙江大学解剖教研室提供。试验方案经医院医学伦理委员会审核通过。

1.2 试验设备 SOMATOM Definition Flash 16排螺旋CT(SIEMENS),Merge eFilm Workstation 2.1.2医学影像浏览和处理软件(Merge),Instron 5569电子万能试验机(Instron),直径3.5mm钛合金螺钉(常州市康辉医疗器械有限公司)。

2 方法

2.1 影像学测定 采用16排螺旋CT机对10名志愿者进行脊柱平扫,扫描范围T_{1~T₈}节段。扫描平

面平行于椎体上、下终板,重建层厚为 0.75 mm,将显示完整的图像数据以 DICOM 格式存储。运用 eFilm Workstation 软件测定各节段的 PRU 途径置钉安全角度范围、椎弓根横径、PRU 横径、椎弓根纵径、PRU 纵径、PRU 重叠纵径。PRU 途径置钉安全角度范围指自横突尖分别向椎管及椎体外侧壁连线的夹角[图 1(1)];椎弓根横径指椎弓根内外侧骨皮质间的最短

距离[图 1(2)];PRU 横径指肋骨外侧骨皮质到椎弓根内侧骨皮质的最短距离[图 1(3)];椎弓根纵径指椎弓根上下骨皮质间的最短距离[图 1(4)];PRU 纵径指在同一节段 PRU,肋骨上缘到椎弓根下缘的最短距离[图 1(5)];PRU 重叠纵径指在同一节段 PRU,肋骨与椎弓根矢状面上互相重叠部分的宽度[图 1(6)]。

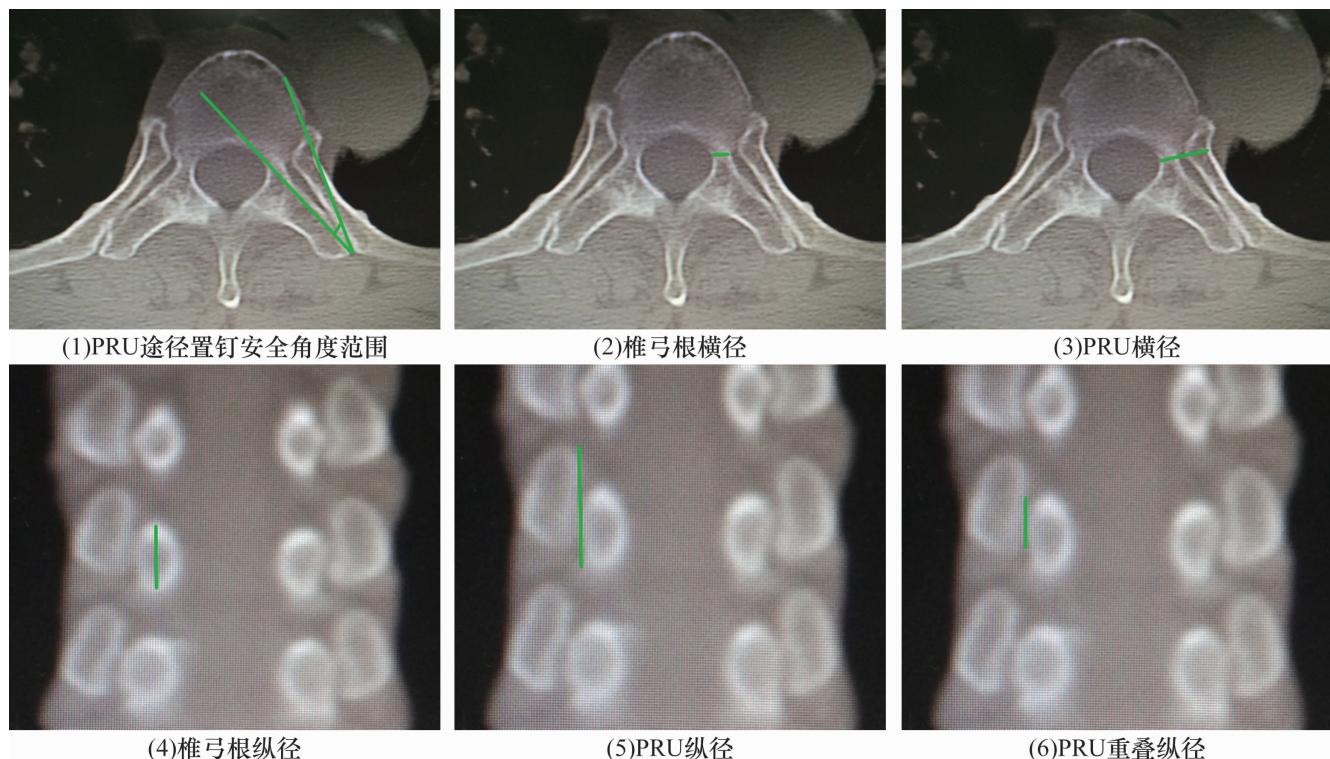


图 1 $T_1 \sim T_8$ 经椎弓根置钉和经 PRU 置钉的影像学指标测量

2.2 生物力学测定 随机于每个脊柱标本的两侧分别经经典椎弓根途径和 PRU 途径置入椎弓根螺钉。经椎弓根途径采用徒手置钉法^[4]置入螺钉,螺钉直径及长度分别为对应的椎弓根横径的 70% 和钉道最长值的 70%^[5]。经 PRU 途径用咬骨钳咬去部分横突尖,以开口器在横突末端肋横突关节头侧开口,锥子沿 PRU 途径中轴线进入肋椎关节直至椎体,用探针测深并探测四周骨质后植入螺钉,螺钉直径与另一侧椎弓根途径置钉螺钉直径相同,螺钉长度为对应 PRU 途径钉道最长值的 70%。将置入椎弓根螺钉的椎体标本置于 Instron 5569 电子万能试验机上进行拔出测试(图 2)。速度设置为 $5 \text{ mm} \cdot \text{min}^{-1}$,最大拉力 3 000 N,最大位移 10 mm^[6]。调整牵拉角度使螺钉以垂直方向拔出,记录从开始到螺钉拔出的曲线图,螺钉大部分拔出即终止测试,曲线的最高峰即最大拔出力记为螺钉的抗拔出力。



图 2 螺钉抗拔出力测定

2.3 数据统计分析 采用 SPSS 13.0 软件进行数据统计分析。10 名志愿者 $T_1 \sim T_8$ 节段椎弓根横径与 PRU 横径的比较、经 2 种途径置入螺钉的抗拔出力的比较采用 t 检验;10 名志愿者 $T_1 \sim T_8$ 椎弓根纵径、PRU 纵径、PRU 重叠纵径三者之间的总体比较采用方差分析,三者之间的两两比较采用 LSD - t 检验。

检验水准 $\alpha = 0.05$ 。

3 结 果

10 名志愿者 $T_1 \sim T_8$ 经 PRU 途径置钉的安全角度范围分别为 $19.71^\circ \pm 1.64^\circ$ 、 $19.42^\circ \pm 1.88^\circ$ 、 $17.17^\circ \pm 0.67^\circ$ 、 $17.22^\circ \pm 1.17^\circ$ 、 $19.36^\circ \pm 1.31^\circ$ 、 $18.67^\circ \pm 1.58^\circ$ 、 $18.82^\circ \pm 2.60^\circ$ 、 $18.72^\circ \pm 1.58^\circ$ 。10 名志愿者 $T_1 \sim T_8$ 椎弓根横径均小于同节段的 PRU 横径(表 1)。10 名志愿者 $T_1 \sim T_8$ 椎弓根纵径、PRU 纵径、PRU 重叠纵径三者之间总体比较,差异均有统计

学意义; $T_1 \sim T_8$ 椎弓根纵径和 PRU 纵径均大于 PRU 重叠纵径 ($P = 0.004, P = 0.003, P = 0.001, P = 0.002, P = 0.013, P = 0.030, P = 0.025, P = 0.001; P = 0.000, P = 0.000$), 椎弓根纵径均小于 PRU 纵径 ($P = 0.000, P = 0.000$); 见表 2。 $T_1 \sim T_8$ 各节段经椎弓根途径置入螺钉的抗拔出力均大于经 PRU 途径(表 3)。

表 1 10 名志愿者 $T_1 \sim T_8$ 椎弓根横径和 PRU 横径 $\bar{x} \pm s, \text{mm}$

横径	样本量 (椎)	T_1	T_2	T_3	T_4	T_5	T_6	T_7	T_8
椎弓根横径	10	8.78 ± 0.05	7.59 ± 0.08	6.29 ± 0.07	5.50 ± 0.05	5.52 ± 0.06	5.90 ± 0.06	6.31 ± 0.07	6.64 ± 0.03
PRU 横径	10	18.23 ± 2.46	16.80 ± 1.31	15.12 ± 1.22	14.43 ± 1.00	14.02 ± 0.85	14.19 ± 1.12	14.77 ± 1.31	15.53 ± 1.90
t 值		18.192	20.175	20.271	27.403	20.312	16.772	14.229	13.000
P 值		0.013	0.002	0.004	0.004	0.001	0.047	0.017	0.048

表 2 10 名志愿者 $T_1 \sim T_8$ 椎弓根纵径、PRU 纵径及 PRU 重叠纵径 $\bar{x} \pm s, \text{mm}$

纵径	样本量 (椎)	T_1	T_2	T_3	T_4	T_5	T_6	T_7	T_8
椎弓根纵径	10	8.04 ± 1.01	10.72 ± 0.99	11.34 ± 0.99	10.67 ± 0.91	10.34 ± 0.94	11.33 ± 0.96	11.30 ± 0.82	11.39 ± 0.78
PRU 纵径	10	11.05 ± 1.83	13.09 ± 1.30	13.45 ± 0.92	12.49 ± 0.94	11.96 ± 0.95	12.36 ± 0.62	12.16 ± 0.71	13.71 ± 1.51
PRU 重叠纵径	10	6.37 ± 0.68	7.46 ± 1.12	8.99 ± 0.62	7.94 ± 0.84	7.96 ± 0.96	7.72 ± 0.88	8.34 ± 0.47	9.34 ± 0.93
F 值		236.422	60.570	67.560	64.965	44.926	85.197	92.350	37.867
P 值		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

表 3 4 具尸体脊柱标本 $T_1 \sim T_8$ 经椎弓根途径和经 PRU 途径置入螺钉的抗拔出力 $\bar{x} \pm s, \text{N}$

置钉途径	样本量 (椎)	T_1	T_2	T_3	T_4	T_5	T_6	T_7	T_8
经椎弓根途径	4	663.60 ± 22.13	702.82 ± 24.23	713.58 ± 37.90	700.70 ± 35.66	805.28 ± 64.67	808.68 ± 42.84	864.62 ± 35.49	909.18 ± 46.05
经 PRU 途径	4	470.33 ± 33.09	531.76 ± 13.53	544.98 ± 14.22	590.80 ± 24.72	591.50 ± 62.55	629.08 ± 43.09	591.60 ± 52.91	640.70 ± 21.41
t 值		27.876	38.402	37.518	10.512	19.546	19.436	24.350	15.162
P 值		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

4 讨 论

上中胸椎经 PRU 途径置钉时首先要确保在安全角度范围内置入螺钉,螺钉置入角度既要大于最小安全角度,又要小于最大安全角度,否则螺钉将偏向内侧进入椎管内损伤胸髓或偏向外侧损伤内脏、大血管等^[7]。由于本研究使用直径 3.5 mm 的螺钉,上中胸椎椎弓根相对较细,经椎弓根置钉时进钉路径基本不可调整,因此研究未测定椎弓根置钉安全角度范围。贺聚良等^[8]通过影像学观察测量脊柱 $T_1 \sim T_4$ 节段,认为 T_3, T_4 椎弓根过于细小,不建议从前方逆向置入椎弓根螺钉,而应选择逆向通过椎体将螺钉置入到 PRU 内。谢陶敢等^[9]通过测量 $T_1 \sim T_{10}$ 的最小内倾角度和最大内倾角度后,认为在的上中胸椎任何节段经

PRU 置钉时均有 $20^\circ \sim 25^\circ$ 的安全范围,较椎弓根置钉大 $10^\circ \sim 15^\circ$,可明显降低手术难度,提高手术安全性。Husted 等^[10-11]通过对正常脊柱胸椎和有脊柱侧凸胸椎的 PRU 及椎弓根进行测量,认为 PRU 在解剖结构上比狭小的椎弓根更适合置入椎弓根螺钉。崔新刚等^[12]的研究发现, $T_1 \sim T_8$ 节段横突与肋骨几乎完全重叠,证实了经 PRU 进钉的可行性。Liljenqvist 等^[13]采用 CT、MRI 对 29 例特发性脊柱侧凸患者的胸椎椎弓根进行了测量,认为狭窄的椎弓根置钉成功率非常低,加之脊柱侧凸往往伴有旋转,更增加了置钉的难度。王欢喜等^[14]发现硬膜囊与上胸椎之间没有任何间隙,经椎弓根置钉风险较大,而经 PRU 途径置钉则更为安全。经肋骨入路穿刺行椎体成形术^[15]已被证

实为一种安全的手术方法,其原理与经 PRU 途径置钉一致。

邢文华等^[16]通过测量尸体标本认为,PRU 纵径的上段实际上没有包括椎弓根,甚至高于椎体的终板,如果上段置入螺钉,几乎没有力学性能;下段完全由椎弓根组成,但椎弓根的外侧没有肋骨阻挡,置入螺钉时可能直接接触或穿破胸膜。因此应将 PRU 纵径的中段,即 PRU 重叠纵径视为复合体的真实有效纵径。

试验中通过对不同节段经 2 种途径置入的椎弓根螺钉的抗拔出力测定,结果表明,在螺钉长度不同,但直径相同的情况下,经椎弓根置入螺钉的抗拔出力明显大于经 PRU 途径置入的螺钉。

本研究的结果提示,上中胸椎经 PRU 途径置入椎弓根螺钉的安全性优于经椎弓根途径,但置入螺钉的稳定性不及后者。

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(2016-09-07 收稿 2016-11-04 修回)

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